

DECEMBER 15, 1918

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# AVIATION AND AERONAUTICAL ENGINEERING



The Thomas-Morse S-4C Scout

VOLUME V  
Number 10

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—PAGE 600—

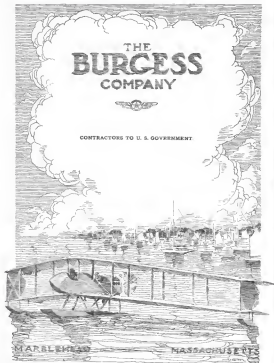
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DECEMBER 15, 1918

## AVIATION AND AERONAUTICAL ENGINEERING

VOL. V, NO. 10

*Member of the Audit Bureau of Circulations*

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## AVIATION AND AERONAUTICAL ENGINEERING

LADISLAV VOSKO  
EDITORIAL BOARD  
GEORGE NEWBOLD  
BUSINESS MANAGER

Vol. V

December 23, 1918

No. 26

**T**HOSE who are awake to the development of the times cannot but wonder at the truly remarkable course aircraft and engine design and production have followed in the United States since our participation in the conflict.

Next to the unbroken series of discontinuity, the richest heritage which this war has left the world is to be found in the wonderful advance made in the aircraft art and overwhelming proof of the practicability of air transportation.

Although pioneers in aviation, America had been up to the time the world war began in 1914, slow to take advantage of its scientific knowledge, almost entirely due to lack of governmental support and support such as was formerly extended by foreign governments to their aircraft engineers. A group of engineers and manufacturers, however, had labored to overcome this backwardness and thus, when the United States entered the war, Washington found available the nucleus of an organization which developed within eight months two one of the three major weapons which we placed at the disposal of humanity—weapons used by land, sea and air.

When the Central Powers had down their arms, America was fast approaching the stage where it would hold undisputed leadership in the air. American built aircraft had gone through the furnace of war, and emerged victorious from the supreme test of reliability, and so had American aircraft, whose gallantry and proficiency it is justice to give due acknowledgment.

At about this time the first American designed fighting aircraft were also beginning to come into their own, showing performance in speed, climb and maneuverability which have demonstrated conclusively that American types of aircraft today are unequaled in the world. This is a statement which no one with a knowledge of the facts will challenge. We have today the best trainer, machine, heavy and light bombers, observation and fighting planes, the most powerful fighters and the lightest fighters per horsepower.

The signing of the armistice was followed by a somewhat hasty reaction, in which a decree was manifested on the part of the various authorities in Washington to curtail war production and accelerate the resumption of normal activities. Inasmuch as the aircraft industry was concerned, there occurred cancellations amounting to over \$300,000,000 affecting every one of the plants which had enabled the United States to take her place among the first-rate flying nations.

While liquidating aircraft contracts, the departments concerned with aviation are going ahead with estimates for simultaneous expenditures during the fiscal year beginning July 1 next. Thus a ledger has been prepared which requests a total of \$165,000,000 for the War Department, of which \$145,000,000 is for aircraft production, and the development of air navigation, and \$20,000,000 for the post office department, while the Navy Department asks the sum of \$25,000,000 for an aircraft program that will be commensurate with its enlarged war budget. The Post Office Department is thoroughly awake to the possibilities of the airplane in the mail service. The Chairman of the Post Office Committee of

the House has just introduced a bill asking \$2,185,000 for the air mail service for the next fiscal year.

Thus Congress is to be asked for a total of \$302,185,000 for the development of air navigation during the fiscal year beginning July 1, next.

But long before any part of these sums shall have become available, the aircraft industry is likely to perish, for, although the Government has still many millions of dollars available for aviation purposes, it apparently fails to recognize the need for providing for the industry between the present, when contracts are being awarded wholesale, and July 1 next, when the new appropriations will be available. Unless a constructive program is immediately formulated and put into effect, the soaring talent industrial genius and financial backing of the aircraft industry will seek other fields. In fact, this process of disintegration has already begun and is proceeding at an alarming rate.

It would indeed be a lamentable lack of foresight if this situation were permitted to develop unchecked. Although conceding that some confusion must attend the shifting of governmental machinery from war time to peace time conditions, there can be no excuse for failure to grasp the magnificent opportunity which is offered America to become supreme in the air, in the military and naval as well as in the commercial field. The war has demonstrated that the airplane is the cheapest form of military and naval weapon and that it is the best, most accurate, most reliable, most accurate and disconcerting action with respect to maintaining a constructive policy, one that will maintain intact the engineering and creative ability now available for brilliant progress in aeronautics, in a word, a policy which will prevent America from sinking back into the decadent place it held in aeronautics before the war.

Those who understand fully the position in which the American aircraft industry now finds itself declare that, unless action is taken at once to insure some of the funds which are available, so that the present critical period may be safely weathered, plants will be forced to close, their invaluable scientific and technical organizations will be scattered to the four winds.

Then, when the various departments seek to develop their aircraft programs after July 1 next, they will be confronted with a depleted industry and will be forced to expend far more money, time and energy on the problem of rehabilitation than an immediate program would call for now.

Here is something which challenges individual thought, not only by the statesman, scientist and manufacturer, but by the average man who, affected by the disaster which threatens flying, has given little heed to the practical varying facts.

To mean what was first said for us by the Leaders, Wrights, Curtiss and Burgesons, to prevent any lapse in the wonderful development which has come out of our aeronautical effort in the war, demands decisive and coordinated action in cooperation with the engineering talent of the industry by all departments of the government which have made or considered tentative plans for utilizing aircraft, otherwise America will lose the place she has won in the air.

# The Boeing Aerodynamical Laboratory

By F. E. McKane

There is so much of talk in the construction of aircraft that, as yet, little as is known as to other lines of aerodynamics, which explains why there should be a devoted effort to obtain the best that research can give. In this connection all of the laboratories through which the world where the laws of aerodynamics are being investigated command the attention of the aircraft manufacturing world. One of the latest laboratories to be completed in this line is the Boeing Aerodynamical Laboratory at Seattle on the campus of the University of Washington.

The laboratory is a gift of Mr. W. R. Boeing, a manufacturer of airplanes in Everett, Wash., to the University of Washington. It shows the building, which is known as the Boeing Aerodynamical Laboratory. This building, because of the war, was held to a secondary wooden structure, although the plans called for a two-story building where students can receive and a one-story building room for a first-class office. The second floor is planned as a large room, to be used jointly, for teaching and research, comprising the whole floor, a space 80 by 25 ft.

The size of the completed section is 80 by 20 ft., with a small basement under the building. This gives a depth of 20 ft. to the chamber which contains the wind channel. The office is at the rear end of the building, extending back to the test room. On the other side of the building, facing the Engineering Hall, which may be seen over the top of the aerodynamic chamber, a door for the entrance leads into the office and the testing chamber. A room the same size as the office, and situated underneath the latter, is used by the students for research. This is separated from the testing chamber by a partition largely of glass to provide light. It will be seen from this illustration that the testing chamber is situated at the rear.

The University campus borders on both Lake Washington and Union, which are connected to Puget Sound by boats. Over them lake full scale testing of airplanes is in progress the year around as the channel and other structures are available all year long. Opportunities for collaboration between the laboratory on the University grounds and the full scale testing done by the Boeing Aircraft Co. seems to be abundant.

## The Testing Chamber

The interior of the testing chamber is shown in Fig. 3. It is seen from the doorway of the calculating room under the office. The full shaped instrument is in the channel in 10 ft. from the partition and the test room. The office above is separated by the main axis of partition so that the centerline of the instrument is a general impression of all laboratory work while in the office above.

A square patch on the ceiling acts as a window and will carry 200 watts per cubic foot. This has not seemed necessary and with the extension of the air in the center of the chamber which will carry 100 watts per cubic foot. The reflection of the ceiling, with mirror surface set into the ceiling so that the reflecting glass is flush with the ceiling. Dr. O'Brien, director of the University of Washington, has been particularly interested in the construction of the lighting apparatus. As a result of his interest, the work in the laboratory can be carried on at night with as little fatigue to the eyes as

in the day time. Even the instruments under the channel can be used easily using only the ceiling lights. The intensity of light varies little in different sections of the room when measured at the same level from the floor. A great amount of light from the ceiling bulbs shines on the floor and the walls of the channel because of glass windows in top, bottom and sides of the channel of the section. The ceiling lights are two main lines in a circuit consisting of the greatest economy in the use of the electricity, at the same time getting a lot through as quickly as possible, so that when the ceiling lights are turned on, the light in the calculating room consists of the light of 1000 watts or more, which is not so much as the ceiling lights. The office above has the same amount of light which is not so much as the ceiling lights. The rest of the lighting system was far lower than for many systems, and for poor illumination results. It is simple, clear and contains no air disturbances as the air is pushed through the channel. The flow of air is not so much as the ceiling lights, with no dropping elements in each duct, so that it is into the place of a free-flowing stream. This is a very important feature of a wind channel testing room.

One of the main considerations in the design of the testing chamber was the feature covering the possibility of continuous testing. Even as much as possible it is most economical to run a test through as quickly as possible, so that when the test is in the use of the channel. This seemed of special importance at the time the laboratory was planned, research in the war demands an air wind channel of great capacity and a small room. To ensure the successful operation of a testing chamber there must be the latest conditions of the testing form on each shift in his latest form. Without this the whole section fails.

## The Wind Channel

The channel proper in general design is like that of all 4 by 6 ft. square tubes, which have been successfully used at the Massachusetts Institute of Technology, Cambridge, Mass., the laboratory of the Curtiss Aeroplane and Motor Corp., Buffalo, N. Y., and the National Physical Laboratory, Teddington, England. The most notable departure from the use of a propeller of 8 ft. diameter, with four blades of low pitch, instead of the usual 7 ft. size. This makes the difference in the end of the room larger and the tube lengthened. An important feature of the channel will show a new rotating and rigid rotation of the channel in a duct of 100 ft. and is finished in steel and polished.

The use of a 6 ft. propeller made the length of the channel and the diameter 10 ft. over all. The tube length is due mainly to the metal tube which connects the air from the square section to that of the propeller. The enlargement of the tube is in two sections. The first consists of the square wooden channel and expands the air from 10 ft. to a round section of 22 ft. 9 in. in a length of 6 ft. 9 in. In an additional feet the cross section expands to the area of a circle of 24 ft. 3 in. diameter, or 6 ft. 9 in. in diameter.

In the mouth of the channel a row of 200 pages, 2 ft. in diameter and 2 ft. 6 in. long, made of bamboo, are stretched as shown in Fig. 2. This unit is made up of narrow sections, each made up of narrow pages. This makes the channel of the air flow smooth, making relatively smooth. These units are brought together and the pages are soldered along these units

using a smooth job throughout. With these units it was possible to get good alignment. The function of these units is to have the air flow parallel from all points in the sides of the channel. The main purpose of this is to make the air flow as nearly as possible of flow in all air be approached. Also, in order to approach this condition, care in the design of the propeller is essential to have an uniform air flow of air, both across the channel and at regular times. A low peak propeller with a large diameter means these conditions. The propeller is of aluminum, made up of five laminations, and is mounted on a standard 3 A. P. hub, both are manufactured by Hall Steel Motor Corp., California.

The propeller drive is the usual shaft drive of the lock box design. The lock shaft to which the propeller is attached runs in two ball bearings at a speed of 1800 rpm. The drive passes between them over a 10-foot speed of 5 ft. 9 in. The bearing housing is made of aluminum, and is made of 1/2 in. only one of the bearings is an 8 ft. 9 in. diameter, so that it is taken care of and for this purpose a New Departure bearing was used in the other 8 ft. 9 in. bearing. By a spring arrangement, provision is made for the shaft to float along the shaft and any movement of the bearings of the motor below is thus made for without jar or vibration.

An important consideration in the design of a wind channel is the matter of being able to hold the propeller revolutions constant during a reading of the instruments at some given speed. It must be possible to vary the speed from 1000 to 1200 rpm, so as to maintain tests at different wind velocities. If direct current is available the rest of the electrical equipment is much simpler. This was not the case at the University of Washington and it was necessary to provide for the conversion of the alternating current, which was done by using a



FIG. 2. THE WIND CHANNEL.

General Electric Co. MFC type motor generator set. This set is shown in Fig. 2 at the far end of the room on a concrete foundation, 22 ft. 9 in. and 22 ft. 9 in. from the floor. It weighs 1000 lb., is 15 ft. capacity, and has a normal speed of 1800 rpm.

The motor which drives the propeller through a silent shaft is an 8 ft. 9 in. adjustable speed motor, which was built by the General Electric Co. This motor is seen under the channel on a foundation 22 ft. 9 in. raised 12 in. from the floor. Two tubes of 1/2 in. in the top of the channel, which are 1/2 in. in diameter, which are 22 ft. 9 in. in diameter. This motor weighs 1400 lb. and has a normal speed of 1800 to 1200 rpm. Its capacity is 15 to 16 ft. non-continuous service.

The wiring from the motor to the generator set is under the



FIG. 3. FRONTIER BALLAST AND WIRE CONTROL.

control floor in metal conduit. Wiring from the control board to the motor is more likely to have alternates made so that this line was run in metal conduit close under the channel.

## The Instruments

The control board and balance arm shown in Fig. 3, as well as the angle unit mechanism, building up the channel. From the metal conduit the wires are shown leading to the control board. From here the wires are connected to the control board and continuing to the resistance under the control board. From here the wires are connected to the instrument board to the various instruments. On this board are placed lamps, solenoid lights. The voltage and current are reported on the instrument. The current is not large as the propeller runs on the shaft, and was being turned over. Resistance, switch and lamp resistance the remainder of the equipment on the instrument board.

The balance which records the wind pressure was constructed by engineers of the Curtiss Aeroplane and Motor Corp. and is similar to the balance used in their own laboratory. The frame holding the remainder of the balance is fastened to the underside of the channel. Between this and the plate glass is a rubber roller for sealing so that an air may enter the channel at this point due to a reduced static pressure inside caused by the propeller motion. The balance passes up through the roller and also the plate glass. On this projecting outside the model under test is placed. In order to prevent any air from entering the channel, a channel is attached to the channel, which is sealed up to the bottom of the glass. By means of brass screws, the balance may be made to pivot either across or along the balance. This takes care of the drag and the lift as the model by the wind motion of balancing weights. There is a disk which allows for the varying of the angle of attack and maintains the angle throughout the reading. There are weights also for primary grade sensitivity.

The installation and building cost approximately \$12,000. In order to prevent alignment of the equipment, the building was adequately supported for testing. It has been found that the amount paid on the floor greatly reduces the amount of dust and dirt which often runs into the air and is pumped around the room. The children required shades to prevent the sun from blinding the research on the channel.

Architects Joe W. R. Boeing were Messrs. Ebb and Gould, of Seattle. The aerodynamical engineering was done by the University of Washington and the instruments have not been completed.

## The Bréguet B-14 All-Metal Airplane

The *Bureau des Ateliers d'Aviation Louis Bréguet*, of Valenciennes, France, are one of the oldest aircraft manufacturing firms in the world, the first having been founded by M. Louis Bréguet, a leading electrical engineer, in 1888. After having experimented for some time with a steam-driven airplane and helicopter machine, with which he actually succeeded in leaving the ground, M. Bréguet produced in 1906 the first motor bi-

plane, but devoted from methodical investigations extending over a period of nearly ten years.

The Bréguet B-14 airplane is a two-seater day-bomber, and is fitted with a 12-cyl., 500 hp. Renault engine, a seven-speed model, the B-17, carries a 600 hp. Renault. Both are tractor engines.

**Wings**—The wings have a tapered stagger of 6.21 in. and a



Bréguet Day-Bomber of the French Air Service  
(C) COURTESY OF PUBLIC INFORMATION

plane and flew it himself at the Reims aviation meeting. This machine was notable for being almost entirely built up of steel tubing. In fact, outside of the wing ribs and some bearing struts in the body, no wood was used in its construction, and the body was sheathed with aluminum.



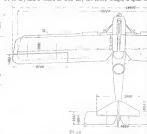
Side Elevation



Front Elevation

Four main, and regardless of various difficulties experienced, M. Bréguet has maintained his faith in all-metal airplane construction, although in his latest machines aluminum alloys have to a large extent displaced steel. The airplane under review is therefore particularly interesting as affording a good example of all-metal construction, based not on recent concep-

ceptions but of 1925 design, both wings are "washed out," the incidence of the upper decreasing from 4.5 deg. at the root, to 2.0 deg. at the tip, while the incidence of the lower wings decreases from 2 deg. to 0 deg. The upper wings have a span of 14.40 m., and a chord of 2.08 m., the lower wings, a span of

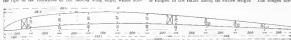


Plan

12.77 m., and a chord of 1.90 m. The chord is constant for both wing throughout the entire length. The upper wings have a dihedral of 175 deg.; the lower ones are straight.

**Wing Spars**—The spars of both wings are drawn double-

end tubes of rectangular section, 65.0 by 34.8 mm. The wall thickness of the spars is 3.6 mm. at the center section, and 1.6 mm. at all other points. The rear spar tapers down toward the tip to the thickness of the lateral wing edge, which con-



The Bréguet Wing Section

tain of 3 mm. web strips reinforced with 3 mm. three-ply wood. At the points where the interplane strut sockets occur, the spars are strengthened by a plugging of ash, of 2 inches, and is welded about one inch down, which are held in place by tubular steel rivets, and serve as a base to the ribs.

The upper front spar is partly plugged at the center section with a cap of pine, 10 mm. thick, which is in turn to one side of the tube by means of small brass screws.

**Interplane Wing Bracing**—Duralumin tubes of 27.38 mm.



Bottom View of Lower Wing with Bracing

diameter are used as compression struts at the interplane strut points, except at the outer points of the lower wings, where duralumin iron ribs are used. These iron ribs also occur on each half-wing, and serve as sparring members. The internal wing frame consists of angle steel webs varying in diameter from 2 to 3 in.

**Ribs**—The ribs are laminated as the spars, and are set parallel with the longitudinal axis of the machine. They are not, however, perpendicular to the wing spars, but follow with the latter an angle corresponding to the washout because the spars are set parallel with the leading edge. The ribs are laminated in some of three-ply planking, resting on the upper side from the leading edge to the front spar, and by two parallel fabric strips, alternately passing above and below the ribs.



Cross Section of Wing Ribs

The main ribs are spaced 3.40 m. apart, and light fabric ribs occur between them at both leading and trailing edges. These fabric ribs are built up of 4 mm. width, while the main ribs are 16 mm. wide. The web of the main ribs are of composite wood, consisting of a central layer of 3 mm. three-ply and two outer layers of birch, the layers are 5 mm. thick.

The wings are surfaced with a fabric of yellowish color, this is sewn onto the ribs, and strengthened with wooden strips when it is exposed to the slip stream. Ribs are provided for the drainage of moisture and equalization of air pressure.

**Aligons and Ryndakons**—Only the upper wings are fitted with aligons, and these are hinged to the rear spar. The

aligons have a span of 374 m. and a chord of 0.82 m.; they are hinged.

On the lower wing the portion situated behind the rear spar is hinged to the latter along its entire length. The aligons are



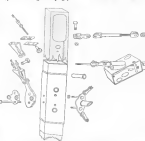
fitted to the upper face of the wing upper web to the top surface of the movable portion, and the latter is maintained at a given angle by the post of twelve rubber cords, which are fixed to the underside of the ribs. The tension of the rubber cords can be adjusted (on the ground) by means of set screws. The object of this arrangement is, of course, to provide in flight for the automatic adjustment of the wing camber to the loading of the airplane.

These "equalizers"—as the movable wing portions may be



Side View of Lower Wing with Equalizers

called the want of a better name—any by the way but a modification of the old Bréguet system of automatic camber control by means of a flexible trailing edge. The pre-war Bréguet airplanes had single wing spars, with a single row of interplane struts, and the incidence of the wings was entirely determined by the tension of springs central inside the wings. With the speed and weight carrying performance of these machines was



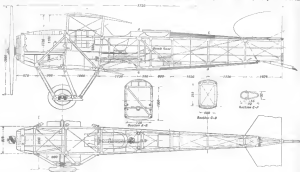
Lower Wing Section for Cable Attachment

quite remarkable—the airplane passengers having been carried for the first time on a Bréguet—the action of the automatic wing control was not always instantly and actually caused several fatal accidents.

\* This term designates in this and the ribs of construction in aviation the thin flexible members here mentioned in the Bréguet, although this could be not properly speaking duralumin.

In view of the fact that it is highly significant that this system should have survived in a modified form on the model B-1 which is one of the most successful day-bombers of the French Air Service, and apparently shows that the value of the aqueduct is more than theoretical, and their mechanism are entirely dependable.

The lengths which connect allions and equalities to the word



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are sheet steel stampings, which are held in place by through bolts. The spars are not plugged at these points.

**Interplate Struts.**—The interplate struts are diamond-shaped of streamline cross section, and fit into dovetail sockets. The inner part of struts are internally strengthened by a continuous channel steel, which is riveted to the sides of the struts.

The diaphragm used in the uniaxial strain has a tensile strength of 40 kg-per sq mm, and an elongation of 18 per cent.

Wires were twisted twice like long wires are. The cables, double, with wooden fibers in between. The leading or gradient wires are 25 mm cables, also twisted in double, and usually connected with one another. The wiring plates are about steel thickness.

**Body.**—The body is almost entirely built up of dendritic tubes, which are joined together, meeting by means of welds (steel tube structure), and are covered with wax. Only at special stressed points, in the front part of the body, have steel tubes been used. The upper and lower sides of the body are covered off by means of clappings. The covering is curved, so as to avoid the corners, where otherwise abrasion is great.

The engine had consists of duralumin levers of V-shape, which are supported by struts of the same metal. All joints are riveted.

The tail planes are built up of welded steel tubing, and are surfaced with canvas. One may note, as a departure from what would seem to be standard French practice, that the elevator is balanced at the tips, somewhat in the fashion of the *Griffon*, although the rudder is unbalanced.

**Undercarriage.**—The undercarriage is of very sturdy construction. It consists essentially of three pairs of horizontal struts of stretched section, which are reinforced internally by

a channel steel member, like the corner irrisplane studs, and are joined by two horizontal steel tubes. The joints are dual steel shoves, and are riveted to the struts. The axle, rubber, spring to the horizontal struts, is a 60 mm steel tube and runs in a cylindrical guide of sheet steel. The streamlining is not as good as the profile, in corner, the struts are not as

The tail shaft is of oak, chauliognis-treated, and concealed at its

tachometer, wiper, alternator, two radiator thermometers, padlocks and indicator arrangement of the gasoline levels, and wipers, all of which are mounted on the instrument board protected by a sheet of Plexiglas glass. To the right of the pilot are mounted: radio-telephone control, starting magnets, gasoline spray pump, fuel starting, gasoline and oil stop cocks, and switches for light lighting and wipers. To the left of the pilot are: throttle and speed levers, air supply control, magnets, switch, and gasoline stop cock.

A third machine gun, for the pilot, is mounted outside of the body, to the left, and is operated by an interrupted gear from the mainshaft.

The observer is seated in the rear cockpit on a hinged seat which swivels him, when not viewing the twin machine guns mounted on a revolving ring, to a search line in the body for the purpose of observing the ground below through the Oboe windows which are fitted to the bottom and sides of his cockpit. The bomb release and wireless control levers are mounted in the seat.

The board magnet is located in the middle of the lower

wings and contains sixteen small bombs, hung in two rows of eight, parallel to the leading edge. The bombs are streamlined in pairs, that is, two lying on the same fore-and-aft axis at a time, by a series of two canards mounted in front of the forward wing spar. The canards are constructed with one member by a pulley and rubber band transmission acting on a transverse shaft, which is operated from the remote control in the observer's cockpit, by means of chains and sprockets. Transmissions fitted with a bellows have

On some of these stripless projects a mode for the carrying of two large bombs inside the pilot's cockpit, but even then the release device is controlled by the observer, the bombs' sight lining in each case mounted on the rear cockpit.

**Weight limits.**—The weight of the D-16, empty, is 1,215 kg. The normal useful load is 314 kg, and the maximum useful load, 638 kg, to which must be added the weight of the fuel, 328 kg. Fully loaded, the machine fires weights 1,945 and 2,045 kg, respectively, which gives, in the former case, a wing loading of about 40 kg per sq m, and a power loading of 6.5 kw. per hp.

### The Aeromarine, Type L, Aeronautical Engine

By Charles F. Willard

With the object of providing a power plant suitable for towing and spotting machines, and approximating that simplicity, sturdiness and durability without undue weight are essential, the Avco-General Motors Plant and Motor Co. has developed a new air-cooled, four-cycle, horizontal engine.

few minutes, allowing inspection of the valve combustion chamber and packing is possible to remove the carbon or grind the valve within the very shortest possible time. The removing and replacement of this head may be accomplished without retaining the motor, due to a special arrangement



*Journal of Management Inquiry*, 19(1), 1-14

known as Type L. The engine, which is water cooled and of the valve-in-the-head type, has cylinders of 4½ in. bore and a stroke of 6½ in. The weight of the engine is 275 lb., and when equipped with electric starter and generator it weighs 400 lb. The rated horsepower is 120 at 1800 r.p.m.

### Crank Case and Colliders

The main portion of the cylinder and cylinder gaskets are integrally cast of aluminum alloy. The type of design eliminates a combination of bolts, screws and flanges, and will give an extremely rigid structure. The cylinder sleeves are also steel forgings, machined all over, to give a uniform wall thickness. After machining, the sleeves are heat treated to the working surface finish. The outside of each sleeve is flange cast in place of the cylinder flange and is cast with the cylinder. The cylinder head gasket is made of an asbestos material. The cylinder head gasket is made of an asbestos material, makes a tight joint against the top flange of each cylinder sleeve. The water joint at the bottom of each sleeve is by industrial cork gasket, which allows freedom for expansion, and at the same time makes a perfectly satisfactory

Cylinder Head and Valve Cover

The cylinder head and valve gear form a complete self-contained unit, which can be removed from the engine in a



Algorithmic. Degree. Expense. Size.

of the splined shaft which drives the camshaft gear. The head is of aluminum alloy with gray iron valve seats cast in position.

The mechanical chambers are machined. The cast-iron body has a large number of ports for the inlet of the spent gases, exhaust valves, guides and valve seats. The design is extremely compact. The same and rollers are housed in, providing possibility of oil cooling the combustion chamber through valve stem guides. There are four valves for each cylinder, two exhaust and two inlet. A special design of valve gear, embodying the multiple link valve arrangement, effects a great reduction in length and weight of valves and valve stems, and also reduces the over-all height of the motor. Each valve train actuates two valves.





# Curtiss

## "THE OPEN BOOK"

### Curtiss Achievements

### *The Great War*

- 1—The design and construction of the fastest fighting airplane ever built. Official Government records credit this triplane, which was built for the U. S. Navy, known as model 26-T, with 160 miles per hour, carrying full military load, pilot and passenger. This is 15 miles per hour faster than any ever claimed for an airplane, a truly earth-breaking achievement, made possible by the development of our new model K motor.
- 2—The design and construction for the Navy of the largest flying boat in the world, colossal crafts capable of carrying five tons useful load. It was one of these boats that recently carried fifty passengers.
- 3—The design and construction for the U. S. Navy of the fastest and most efficient Seaplane in service anywhere. This craft, which is known as the Curtiss model H-A, with Liberty motor, made an official speed of 146 miles per hour with full military load, armament, ammunition, pilot and passenger.

The development and construction of a 12 cylinder, 400 H.P. motor of an entirely new and much lighter type, known as the Curtiss model K-12. These motors have undergone exhaustive tests and are already in production.

The development and construction of the Curtiss model K-6, a new and much lighter 6 cylinder motor. This engine develops 160 H.P. and possesses greatest endurance and reliability.

The development and construction on a large scale of the Curtiss OXK motor and the J-N-3 training planes, which were used almost exclusively by the United States and Canada and largely in England for the training of American and British aviators. The training of our war-time leaders of the original land and marine flying pilots, most of whom entered the service and formed the nucleus of the United States Naval Training Force.



The Curtiss Engineering Corporation is today the center of aircraft development. Glenn H. Curtiss and his engineers have been busy carrying forward the production of suitable commercial types. Aircraft are already available, and are as superior in design, workmanship and performance.

**CURTISS ENGINEERING CORPORATION, GARDEN CITY, L. I.**

Its airplanes, instead of being decreased, will be increased by the increased requirements, and they are perfecting designs and designs for sportsman's use, mail carrying and other peace-time purposes. Curtiss military planes have proved themselves to be.

**Tensile Properties.** The value of tensile strength as a measure of the quality of an ordinary textile material has long been realized, and it was largely the fact that this value was easily measured, which aided recognition of nylon airplane fabrics.

An airplane wing covering, for purposes of this discussion, may be considered as a flat, rectangular sheet supported on fair sides and subjected to pressure which may be considered as uniformly distributed over an area defined by the width of the rib spacing in one direction and relatively small distance

load-stretch relations. The term shrinkage has been applied to refer to fabric tensions and leads to confusion as to the nature of the shrinkage. It has been observed that the fabric having the least stretch at the time loads are applied after drying, and that a plain woven fabric is stiffer than a fabric woven with fewer interstices and having less stretch. The fabric tension is dependent largely upon the support, which the fabric loads to the same level as the complete wing with the dope binds the yarns together in their crimped condition, and is dependent only slightly on the shrinkage.

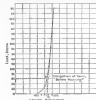


FIG. 5. GRAPH OF AN ARBITRARY YARN OF COTTON AND MULTIPLE STRUCTURES

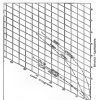


FIG. 6. LOAD-STRETCH RELATIONS OF STANDARD ENGLISH THREAD & AIRPLANE LINEN

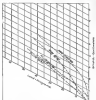


FIG. 7. LOAD-STRETCH RELATIONS OF STANDARD & DRESS COTTON FABRICS

in the other direction. The stress in the material of the action being considered is a function of the resistance of the fabric of extension plus a factor involving what is usually termed as an axial tension load. The resistance at any given pressure is determined by the load-stretch relations of the material, and although the load-stretch diagram does not consider the effect of axial loading, it does serve as a very valuable index to relative factors of safety of the various materials. The wing covering must be airtight in order that the pressure may not build up and cause fabric stress and that flight efficiency may not be lowered. The material must remain weightless as long as the dope film is not ruptured or deteriorated.

The life of a fabric may be considered to be dependent upon the life of the dope. The dope may be caused to become deteriorated either by repeatedly exceeding its elastic limit or by

The intensity of fabric tension is believed to be largely dependent upon the psychology of the flyer, but, with the present dope, fabric toughness is almost synonymous with life of the dope or fabric.

It is believed that the fatigue properties of a fabric may be related either definitely to the shape and area of the hysteresis loop. Although these phases of the investigation is not entirely complete, the area of the hysteresis loop has been used to predict the fatigue properties of the materials with a large degree of accuracy.

The relative recoverable stretch of an airplane wing covering is quite readily indicated from an examination of the hysteresis loops of the load stretch diagrams. It was not intended to convey the idea that all degrees of wing-covering looseness were equally desirable, and in the absence of exact data on the effect of fabric looseness on lift and drag, the allowable lack of recoverable stretch must be left to the judgment of the investigator.

The effect of the amplitude of the vibrations of a wing covering is, after dry dope, determined by the recoverable stretch of the material, and here again the phase of the investigation is not complete and the magnitude of this property must be left to the judgment of the investigator.

**First Resistance, Tensile Method.** This method of determining tear resistance has been considered less applicable to wing-covering materials, as the value of the load-stretch relations is not fully realized, and has been superseded by the bursting-test method. The method may be used, however, in cases where the samples are too small for bursting test and when such apparatus is not readily obtainable.

**Resistance to Uniformly Distributed Pressure.** As has been already pointed out, the stress in an airplane covering material is a function of the curvature of the material in any given direction. It has been observed that the tensile strength is improved by plotting airfoil-shaped surface means against stretch of the material, during the application of pressure does not agree with the load stretch diagram, the difference is probably due to the relaxed stress in the draped fabric and is fit fact that the end and side effects of the tension strips are not present in the present test.

The test does not take the effect of loosening into account much from wing deflection, but does serve as a more valuable index to factors of safety than the conventional tensile test.

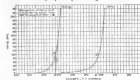


FIG. 8. TYPICAL TEST OF CREEP ON YARN-LENGTH RELATIONS showing it is determining type of fabric. The better condition may be related to a measure by testing the material with permanent stretch or dope which is applied to the determining portion of the specimen. (This development may be obtained in an English investigation.)

The shape of the hysteresis curves of the draped fabric serves as a valuable index as to whether the elastic limit of the dope will become exceeded under conditions of flight.

The ability of a fabric to stretch depends largely upon its

From the pressure-deflection curves it is easier to visualize the relative effect of wing deflection. The true condition of flight are not duplicated, but the effects of the two systems of yarns investigated and the results are less deceptive than those obtained from tensile tests.

**Bursting Test First.** This test, like the bursting test, is a much better index to relative factors of safety than tensile tests. Questions of fabric reinforcement and balance of fabric are readily solved by a careful interpretation of the results obtained from such a test.

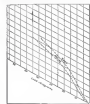


FIG. 9. LOAD-STRETCH DIAGRAM OF A 2.6% UNMERCERIZED RAYON DOPES

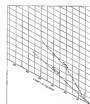


FIG. 10. LOAD-STRETCH DIAGRAM OF A 2.6% MERCERIZED RAYON

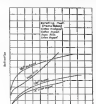


FIG. 11. DESCRIPTION OF CENTER POINT OF FABRIC WHEN SUBJECTED TO AIR PRESSURE

#### Results of Tests

It is proposed to give typical examples of tests performed on satisfactory and unsatisfactory fabrics in order that the value of the tests may be more readily realized.

**Length of Yarn and Crimp.** A typical set of crimp or yarn-length readings is shown in Fig. 8. It will be noted that the hysteresis relations follow a straight-line ratio after a particular tension is reached. It is assumed that the yarn has adjusted itself after this point is reached, and that if it were not crimped the relations would start below this point.

Fig. 9 shows the crimp of an average yarn of coarse and multiple structure. Consequently the yarn and there are as many as six of a tangled condition, as is shown by the lower part of the curve.

**Tensile Properties.** The load-stretch relations of a standard English thread & airplane linen are shown in Fig. 6. It will be noted that the draped-fabric curve is practically a straight line, the draped yarn curve shows a distinct yield point, as is indicated by the reversal of the curvature of the fabric.

Fig. 7 represents the load-stretch relations of a standard grade cotton fabric, which curve, it will be observed, is very similar to that of the linen fabric.

The load stretch diagrams of a fabric may be divided into three parts according to the preponderant influences as they appear postures: (a) crimp, (b) crimp and yarn, (c) yarn characteristics. Referring to the yarn load-stretch diagram of the cotton fabric, Fig. 7, the part of the curve extending to approximately 2 lb. is influenced almost entirely by crimp, the curve from 2 to 30 lb. by yarn and crimp, the curve from this point on shows the characteristics of the yarn in the crimped condition.

This analysis suggests the particular part of the load-stretch diagram which should be varied to produce the desired shape of curve. The part of the curve below 30 lb. may be varied by changing the weave structure, stiffness of the yarn, and more particularly tension, or the yarn during and after it at the point as determined by the water dope test, and the relative magnitudes of the respective stretches of the warp and filling are determined by loom tensions.

Fig. 8 represents the load-stretch diagram of a 2.6% mercerized rayon dope. Both the warp and filling show a dope yield point between 0 and 30 lb. as is represented by the reversal of the curvature of the diagram.

The same construction of fabric made of mercerized rayon is represented by the load-stretch diagram, Fig. 10. The filling diagram does not show a reversal of curvature and the elastic limit of the dope will not be exceeded under normal conditions of flight. Service tests on these latter two fabrics showed that the mercerized fabric became somewhat crinkly after

a short period while the mercerized-rayon fabric stood dry very well. Similar tests on fabrics of various load-stretch diagrams showed that the fabrics whose draped-filling load-stretch diagrams were generally straight lines stood up exceptionally well.

The magnitudes of the strength and the looseness of the nylon fabrics are dependent upon the completeness with which the dope penetrates the fabric and the completeness with which the dope is extracted from desiccating solvents such as light and heavier.

The dope penetration of the 3.6% fabric, 18 square, plain weave, is extensive, the dope penetration of the 2.6% mercerized fabric is slightly more than that of the standard linen fabric. Relative penetration of the dope reduces the tear resistance materially. If the standard 2.6% fabric is woven in a 2 to 2 basket, the dope penetration is such as to cause an extremely low tear resistance. The small crimp in such a fabric makes it dope up very rapidly.

**Bursting Test.** The curves, Fig. 11, represent the pressure-deflection properties of the center point of the fabric when subjected to air pressure, as previously described. The deflection at any load of the fabric subjected is higher than that of the dope film. The deflection of the dope film is less than the deflection of either the fabric or the film. This further substantiates the theory that tension is produced by the dope contracting the yarn in three unequal conditions, and that in the standard fabric the elastic limit of the dope is not exceeded. It will be observed that the nylon fabric is capable of resisting more pressure than the linen, and it will have, therefore, a higher factor of safety. The fabric tension is practically the same as that of the linen.

**First Resistance.** From an examination of the direction of the yarn about a twist, it is concluded that the true resistance is a function of the strength of the individual yarn and the number being stressed. The number of yarns being stressed is dependent upon the load-stretch relations of the fabric and the weave structure. In the case of the nylon and mercerized rayon fabrics, the true resistance, let us consider two fabrics: (a) Standard 2.6% mercerized, 80 square, plain weave, (b) 2.6% mercerized yarn, 80 square,





### Liberty Fuel Cheaper Than Gasoline

Major G. B. Zimmerman, Director of the War Department's research and development division, has given out some facts about "Liberty" fuel, discovered by army engineers and described as vastly cheaper than gasoline and having more power.

The new fuel oil, which will soon be on the market, was discovered after five months of experimentation by army officials on the question of gasoline for motor power. Its basis is kerosene, with other ingredients of a few cast, and produced in quantity in this country. The process of manufacture is exceedingly simple, and the fuel can be used in all kinds of motor-driven vehicles.

Major Zimmerman, who with Capt. R. C. Wengert, of the gas and oil production division of the War Department, is credited with the new discovery, announced its advantages as follows:

- It will start easier than gasoline.
- Leaves no residue of carbon, soot, etc.
- Expands at temperatures below zero.
- Is capable of greater mileage per gallon than gasoline.
- Holds against pressure in pipelines, requiring only four pump or flange.
- Its combustion requires less oxygen than gasoline.

Can be manufactured for less money than gasoline.

It can be used in automobiles without any change in the carburetor and without detriment to the car.

Developed in one United States engine, it has shown itself superior to gasoline as an airplane fuel. It has 17 per cent higher fuel economy than export gasoline.

One of the Bureau of Standards' reports showed that a five-ton truck ran 200 miles on one gallon of gasoline and a gallon of gasoline, 61.5 miles a quart for transportation and a half gallon of water. With Liberty fuel the truck averages a gallon of fuel, 102.1 miles a quart of transporting oil and two gallons of water.

### Leeming's Monoplane a Success

Major Gen. William L. Keady, Director of Military Aeronautics, has authorized the receipt of information from Dayton, Ohio, that the Leeming two-seater monoplane in recent tests there developed 145 m. p. h., with full military load, including four guns, which is in excess of any record made by a European single-seater scout machine. The Leeming plane in these tests developed 20,000 ft., carrying two passengers.

This machine is equipped with a 500 hp. Armstrong-Hughes engine built by the War Department.

The design of the machine is entirely original and a distinct American development which has finally been declared competent to be of national importance. It will be brought out. The completion of the machine for the purpose of production is such that it requires one-tenth the number of parts of the ordinary European design. All war steps have been eliminated and the monoplane type of structure for the first time revealed an strong and rigid as any airplane without having any of the well-known advantages of the monoplane.

### To Encourage Trans-Atlantic Flight

To encourage a trans-Atlantic flight by an American designed and built airplane, Louis M. Upson, president of the Aeromarine Plane and Motor Corporation, has written and sent to W. F. Willard, his chief engineer, to investigate the company's willingness to undertake the design and construction of a machine capable of accomplishing this flight for any individual, organization or company, at actual cost of material and labor only. Mr. Upson, who has already been prominent in promoting biplanes, automobiles and flying cars, believes that when such steps are taken at once in this country, as England, France, Belgium or even Germany, airplanes will be first to cross the Atlantic. This view is adopted to be based on first-hand knowledge obtained by Mr. Willard during his recent trip to Europe at a request of an American and American commission sent over by the Government.

### Test Trip of the Christmas Plane

A new airplane, the invention of Dr. William W. Chittenden of Washington, D. C., was tried out at Central Park on the east end of Hempstead Plaza December 2.

### C. F. Kemerling's Dinner Engagement

Calling up New York City from Dayton, Ohio, at 10 o'clock in the morning, making an engagement for dinner and the theater in the metropolis for that evening and keeping it, was the exploit November 20th of C. F. Kemerling, representative of the Dayton-Wright Airplane Co. and president of the Society of Automobile Engineers, and Harold H. Hamilton, chief pilot of that company. The next day they came to Washington in a representative of the same line.

Headings of all run-up airplane flight records in the United States was necessary in order that they arrive in time.

The trip was made in a De Havilland-4 army plane equipped with a 120-horsepower, 400-hp. Liberty engine.

From the time the big two-seater arose from the experimental field south of the plant in Dayton until it was posted in one of the hangars at the Marine Flying Field, near New York, just four hours and ten minutes elapsed. The distance from Dayton to New York is 300 miles. Slightly more than 134 miles an hour was the average for the trip.

### Fifty Passengers on the NC-1

It is announced from Washington that an NC-1 plane of the United States Navy broke the world's record for passenger-carrying capacity at the Naval Air Station, Rockaway, N. Y., on November 27, when a flight was made with fifty men on board. For the special purpose of demonstrating the plane's lifting capacity, Lieut. David R. McDougall, U. S. N. A. F. C., was the pilot.

The NC-1 is the first American flying boat with two Liberty engines which develop a maximum of 1200 hp., and gave a cruising speed of about 80 m. p. h.

The design and construction of the NC-1, with its triple engines, large size and other distinctive features, was carried out by the Navy in cooperation with the Curtiss Engineering Corp.

The NC-1 made her trip from Rockaway to Washington, about 250 miles, in 2 hours and 30 minutes.

### Changes in the Dept. of M. A.

Col. Arthur Woods has been appointed Assistant Director of Military Aeronautics. Colonel Woods, who was Chief of the Aeronautics Division of Military Aeronautics, is the immediate successor of Col. Gerald C. Hoad. The appointment of Colonel Woods, however, was only temporary, and therefore is in accordance with the provisions of the Act. Colonel Woods is the immediate successor of Col. Henry H. Arnold.

Colonel Hoad has been appointed chairman of a Board to work out and recommend plans for the permanent organization of the air force.

Colonel Woods has been succeeded as Chief of the Personnel Section by Lieut. Col. Hugh B. Loomis, formerly Executive Officer of that section.

### Gleat Martin Breaker's Flight

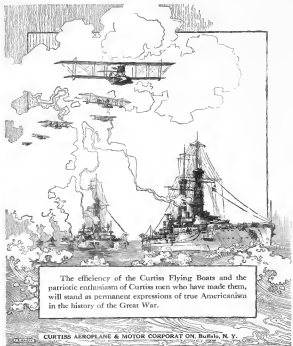
A big Glenn Martin deep-sea plane, which left its base at Hampton, Va., on its Atlantic run to Washington, arrived at 12:30 the next day at Bolling Field, having been delayed over night at Annapolis near Potomac, Pa., by a snow storm. The big big of the military and the first one to fly from Washington—was made in one hour and fifteen minutes, which included a climb through snow clouds to an elevation of 12,000 ft.

Major Harley W. Zelen, pilot, who acted as observer and co-pilot for the Division of Military Aeronautics, stated that this is the fastest flight ever made by a machine of this type.

### No Licenses for Civilian Nav

Inquiry at the War and Navy departments brings out the fact that no civilian flying license is required by the Red Cross and manufacturers' test pilots for the Army and Navy.

It is unlikely that there will be any modification of the order for some time to come.



## The Air Transport Number of Aviation and Aeronautical Engineering

January 1, 1919

will present:

All available information bearing upon the policy of the United States for its permanent military aeronautical establishment and the plans of the Post Office Department, Reclamation and Forestry Services, Coast Patrol and Geodetic Survey, etc.

Plans of the manufacturers for creating a commercial demand.

Special articles which will contain a fund of information and suggestions as to possible markets for American aircraft in the United States and abroad, and how to reach those markets. Views of the leading men of the industry, of Government officials, army and navy officers, as well as representative opinions from possible purchasers of aircraft for sporting and utilitarian purposes.

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149000 to 150000 ft. pressure, 755 to 760 lb. per sq. in. and 150000 to 151000 ft. pressure, 760 to 765 lb. per sq. in. and 151000 to 152000 ft. pressure, 765 to 770 lb. per sq. in. and 152000 to 153000 ft. pressure, 770 to 775 lb. per sq. in. and 153000 to 154000 ft. pressure, 775 to 780 lb. per sq. in. and 154000 to 155000 ft. pressure, 780 to 785 lb. per sq. in. and 155000 to 156000 ft. pressure, 785 to 790 lb. per sq. in. and 156000 to 157000 ft. pressure, 790 to 795 lb. per sq. in. and 157000 to 158000 ft. pressure, 795 to 800 lb. per sq. in. and 158000 to 159000 ft. pressure, 800 to 805 lb. per sq. in. and 159000 to 160000 ft. pressure, 805 to 810 lb. per sq. in. and 160000 to 161000 ft. pressure, 810 to 815 lb. per sq. in. and 161000 to 162000 ft. pressure, 815 to 820 lb. per sq. in. and 162000 to 163000 ft. pressure, 820 to 825 lb. per sq. in. and 163000 to 164000 ft. pressure, 825 to 830 lb. per sq. in. and 164000 to 165000 ft. pressure, 830 to 835 lb. per sq. in. and 165000 to 166000 ft. pressure, 835 to 840 lb. per sq. in. and 166000 to 167000 ft. pressure, 840 to 845 lb. per sq. in. and 167000 to 168000 ft. pressure, 845 to 850 lb. per sq. in. and 168000 to 169000 ft. pressure, 850 to 855 lb. per sq. in. and 169000 to 170000 ft. pressure, 855 to 860 lb. per sq. in. and 170000 to 171000 ft. pressure, 860 to 865 lb. per sq. in. and 171000 to 172000 ft. pressure, 865 to 870 lb. per sq. in. and 172000 to 173000 ft. pressure, 870 to 875 lb. per sq. in. and 173000 to 174000 ft. pressure, 875 to 880 lb. per sq. in. and 174000 to 175000 ft. pressure, 880 to 885 lb. per sq. in. and 175000 to 176000 ft. pressure, 885 to 890 lb. per sq. in. and 176000 to 177000 ft. pressure, 890 to 895 lb. per sq. in. and 177000 to 178000 ft. pressure, 895 to 900 lb. per sq. in. and 178000 to 179000 ft. pressure, 900 to 905 lb. per sq. in. and 179000 to 180000 ft. pressure, 905 to 910 lb. per sq. in. and 180000 to 181000 ft. pressure, 910 to 915 lb. per sq. in. and 181000 to 182000 ft. pressure, 915 to 920 lb. per sq. in. and 182000 to 183000 ft. pressure, 920 to 925 lb. per sq. in. and 183000 to 184000 ft. pressure, 925 to 930 lb. per sq. in. and 184000 to 185000 ft. pressure, 930 to 935 lb. per sq. in. and 185000 to 186000 ft. pressure, 935 to 940 lb. per sq. in. and 186000 to 187000 ft. pressure, 940 to 945 lb. per sq. in. and 187000 to 188000 ft. pressure, 945 to 950 lb. per sq. in. and 188000 to 189000 ft. pressure, 950 to 955 lb. per sq. in. and 189000 to 190000 ft. pressure, 955 to 960 lb. per sq. in. and 190000 to 191000 ft. pressure, 960 to 965 lb. per sq. in. and 191000 to 192000 ft. pressure, 965 to 970 lb. per sq. in. and 192000 to 193000 ft. pressure, 970 to 975 lb. per sq. in. and 193000 to 194000 ft. pressure, 975 to 980 lb. per sq. in. and 194000 to 195000 ft. pressure, 980 to 985 lb. per sq. in. and 195000 to 196000 ft. pressure, 985 to 990 lb. per sq. in. and 196000 to 197000 ft. pressure, 990 to 995 lb. per sq. in. and 197000 to 198000 ft. pressure, 995 to 1000 lb. per sq. in. and 198000 to 199000 ft. pressure, 1000 to 1005 lb. per sq. in. and 199000 to 200000 ft. pressure, 1005 to 1010 lb. per sq. in. and 200000 to 201000 ft. pressure, 1010 to 1015 lb. per sq. in. and 201000 to 202000 ft. pressure, 1015 to 1020 lb. per sq. in. and 202000 to 203000 ft. pressure, 1020 to 1025 lb. per sq. in. and 203000 to 204000 ft. pressure, 1025 to 1030 lb. per sq. in. and 204000 to 205000 ft. pressure, 1030 to 1035 lb. per sq. in. and 205000 to 206000 ft. pressure, 1035 to 1040 lb. per sq. in. and 206000 to 207000 ft. pressure, 1040 to 1045 lb. per sq. in. and 207000 to 208000 ft. pressure, 1045 to 1050 lb. per sq. in. and 208000 to 209000 ft. pressure, 1050 to 1055 lb. per sq. in. and 209000 to 210000 ft. pressure, 1055 to 1060 lb. per sq. in. and 210000 to 211000 ft. pressure, 1060 to 1065 lb. per sq. in. and 211000 to 212000 ft. pressure, 1065 to 1070 lb. per sq. in. and 212000 to 213000 ft. pressure, 1070 to 1075 lb. per sq. in. and 213000 to 214000 ft. pressure, 1075 to 1080 lb. per sq. in. and 214000 to 215000 ft. pressure, 1080 to 1085 lb. per sq. in. and 215000 to 216000 ft. pressure, 1085 to 1090 lb. per sq. in. and 216000 to 217000 ft. pressure, 1090 to 1095 lb. per sq. in. and 217000 to 218000 ft. pressure, 1095 to 1100 lb. per sq. in. and 218000 to 219000 ft. pressure, 1100 to 1105 lb. per sq. in. and 219000 to 220000 ft. pressure, 1105 to 1110 lb. per sq. in. and 220000 to 221000 ft. pressure, 1110 to 1115 lb. per sq. in. and 221000 to 222000 ft. pressure, 1115 to 1120 lb. per sq. in. and 222000 to 223000 ft. pressure, 1120 to 1125 lb. per sq. in. and 223000 to 224000 ft. pressure, 1125 to 1130 lb. per sq. in. and 224000 to 225000 ft. pressure, 1130 to 1135 lb. per sq. in. and 225000 to 226000 ft. pressure, 1135 to 1140 lb. per sq. in. and 226000 to 227000 ft. pressure, 1140 to 1145 lb. per sq. in. and 227000 to 228000 ft. pressure, 1145 to 1150 lb. per sq. in. and 228000 to 229000 ft. pressure, 1150 to 1155 lb. per sq. in. and 229000 to 230000 ft. pressure, 1155 to 1160 lb. per sq. in. and 230000 to 231000 ft. pressure, 1160 to 1165 lb. per sq. in. and 231000 to 232000 ft. pressure, 1165 to 1170 lb. per sq. in. and 232000 to 233000 ft. pressure, 1170 to 1175 lb. per sq. in. and 233000 to 234000 ft. pressure, 1175 to 1180 lb. per sq. in. and 234000 to 235000 ft. pressure, 1180 to 1185 lb. per sq. in. and 235000 to 236000 ft. pressure, 1185 to 1190 lb. per sq. in. and 236000 to 237000 ft. pressure, 1190 to 1195 lb. per sq. in. and 237000 to 238000 ft. pressure, 1195 to 1200 lb. per sq. in. and 238000 to 239000 ft. pressure, 1200 to 1205 lb. per sq. in. and 239000 to 240000 ft. pressure, 1205 to 1210 lb. per sq. in. and 240000 to 241000 ft. pressure, 1210 to 1215 lb. per sq. in. and 241000 to 242000 ft. pressure, 1215 to 1220 lb. per sq. in. and 242000 to 243000 ft. pressure, 1220 to 1225 lb. per sq. in. and 243000 to 244000 ft. pressure, 1225 to 1230 lb. per sq. in. and 244000 to 245000 ft. pressure, 1230 to 1235 lb. per sq. in. and 245000 to 246000 ft. pressure, 1235 to 1240 lb. per sq. in. and 246000 to 247000 ft. pressure, 1240 to 1245 lb. per sq. in. and 247000 to 248000 ft. pressure, 1245 to 1250 lb. per sq. in. and 248000 to 249000 ft. pressure, 1250 to 1255 lb. per sq. in. and 249000 to 250000 ft. pressure, 1255 to 1260 lb. per sq. in. and 250000 to 251000 ft. pressure, 1260 to 1265 lb. per sq. in. and 251000 to 252000 ft. pressure, 1265 to 1270 lb. per sq. in. and 252000 to 253000 ft. pressure, 1270 to 1275 lb. per sq. in. and 253000 to 254000 ft. pressure, 1275 to 1280 lb. per sq. in. and 254000 to 255000 ft. pressure, 1280 to 1285 lb. per sq. in. and 255000 to 256000 ft. pressure, 1285 to 1290 lb. per sq. in. and 256000 to 257000 ft. pressure, 1290 to 1295 lb. per sq. in. and 257000 to 258000 ft. pressure, 1295 to 1300 lb. per sq. in. and 258000 to 259000 ft. pressure, 1300 to 1305 lb. per sq. in. and 259000 to 260000 ft. pressure, 1305 to 1310 lb. per sq. in. and 260000 to 261000 ft. pressure, 1310 to 1315 lb. per sq. in. and 261000 to 262000 ft. pressure, 1315 to 1320 lb. per sq. in. and 262000 to 263000 ft. pressure, 1320 to 1325 lb. per sq. in. and 263000 to 264000 ft. pressure, 1325 to 1330 lb. per sq. in. and 264000 to 265000 ft. pressure, 1330 to 1335 lb. per sq. in. and 265000 to 266000 ft. pressure, 1335 to 1340 lb. per sq. in. and 266000 to 267000 ft. pressure, 1340 to 1345 lb. per sq. in. and 267000 to 268000 ft. pressure, 1345 to 1350 lb. per sq. in. and 268000 to 269000 ft. pressure, 1350 to 1355 lb. per sq. in. and 269000 to 270000 ft. pressure, 1355 to 1360 lb. per sq. in. and 270000 to 271000 ft. pressure, 1360 to 1365 lb. per sq. in. and 271000 to 272000 ft. pressure, 1365 to 1370 lb. per sq. in. and 272000 to 273000 ft. pressure, 1370 to 1375 lb. per sq. in. and 273000 to 274000 ft. pressure, 1375 to 1380 lb. per sq. in. and 274000 to 275000 ft. pressure, 1380 to 1385 lb. per sq. in. and 275000 to 276000 ft. pressure, 1385 to 1390 lb. per sq. in. and 276000 to 277000 ft. pressure, 1390 to 1395 lb. per sq. in. and 277000 to 278000 ft. pressure, 1395 to 1400 lb. per sq. in. and 278000 to 279000 ft. pressure, 1400 to 1405 lb. per sq. in. and 279000 to 280000 ft. pressure, 1405 to 1410 lb. per sq. in. and 280000 to 281000 ft. pressure, 1410 to 1415 lb. per sq. in. and 281000 to 282000 ft. pressure, 1415 to 1420 lb. per sq. in. and 282000 to 283000 ft. pressure, 1420 to 1425 lb. per sq. in. and 283000 to 284000 ft. pressure, 1425 to 1430 lb. per sq. in. and 284000 to 285000 ft. pressure, 1430 to 1435 lb. per sq. in. and 285000 to 286000 ft. pressure, 1435 to 1440 lb. per sq. in. and 286000 to 287000 ft. pressure, 1440 to 1445 lb. per sq. in. and 287000 to 288000 ft. pressure, 1445 to 145





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against the integrity of an assemblage of metal parts and the question of the bearing's quality becomes a defense thing. And in aeroplanes the make is all that—and more. So the use of bearings in such service becomes the most vital consideration for their makers. In this respect it's interesting to note that Hess-Bright Ball Bearings are fit to serve.

For, in addition to all the usual qualities of average ball bearings, the Hess-Bright Product has unusual wearing power—due entirely to exceptional choice of metal for their making combined with painstaking care in their finish. They stand excessive strain and stress with unflinching dependability. It is this that has made them standard.

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Model O X 5 Curtiss motor equipped  
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"Think of the  
Consequences"



This caution, displayed at the Aviation Training Shops, is the beacon that warns against carelessness. An overheated or improperly lubricated bearing may be the cause of sending the best-built airplane crashing to the earth. SKF equipped airplanes are not subject to hot bearings, nor will SKF bind when reversements and spinning nose dives cause the whole structure to rack and creak. SKF Ball Bearings are self-aligning.

**SKF BALL BEARING CO.**  
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